

## Lecture: Mon 10/31

## 1. Electromagnetic vector fields

- Let  $g(x, y) = (r(x, y), s(x, y))$  be any vector field.
- Divergence of  $g$  measures rate of outflow from each point:

$$\operatorname{div} g(x, y) := \frac{\partial r}{\partial x} + \frac{\partial s}{\partial y} = r_x(x, y) + s_y(x, y).$$

- Curl of  $g$  measures counter-clockwise torque (rotational force) around each point:

$$\operatorname{curl} g(x, y) := \frac{\partial s}{\partial x} - \frac{\partial r}{\partial y} = s_x(x, y) - r_y(x, y).$$

- An electric force field  $g(x, y)$  satisfies Maxwell's equations: the curl and divergence must vanish at all points:

$$\operatorname{curl} g(x, y) = \operatorname{div} g(x, y) = 0.$$

That is:

$$\text{(Maxwell)} \quad r_x = -s_y \quad , \quad r_y = s_x.$$

These equations hold in a region with no charge present. In general,  $\operatorname{div} g$  is the charge density at each point.

## 2. Complex analytic vs electric vector fields

- Let  $f(x + iy) = u(x, y) + i v(x, y)$  be complex analytic, meaning it satisfies:

$$\text{(Cauchy-Riemann)} \quad u_x = v_y \quad , \quad u_y = -v_x.$$

- *Proposition:* Given  $f(x + iy)$ , let  $g(x, y)$  be the complex conjugate vector field:  $g(z) := \overline{f(x + iy)}$ ,

$$g(x, y) := (u(x, y), -v(x, y)).$$

Then clearly:

$$f(x, y) \text{ complex analytic} \iff g(x, y) \text{ satisfies Maxwell.}$$

- *Example:*  $f(z) = z$ ,  $g(x, y) = (x, -y)$ . Then  $f(z)$  is analytic everywhere and  $\text{curl } g = \text{div } g = 0$ .
- *Example:*  $f(z) = 1/z$ ,

$$g(x, y) = \frac{(x, y)}{x^2 + y^2} = \text{point-charge},$$

an outward force proportional to inverse of distance (which is the 2-dimensional version of Coulomb's Law). Then  $f(z)$  is analytic except at the origin, and  $g(x, y)$  satisfies Maxwell except at the origin, where there is a point-charge with infinite charge-density:  $\text{div } g(0, 0) = \infty$ .

- *Example:*  $g(z) = (x, y)$  corresponds to  $f(z) = \bar{z}$ . Then  $f(z)$  is *not* analytic, and  $g(x, y)$  does *not* satisfy Maxwell's equations, since  $\text{curl } g(x, y) = 0$  but  $\text{div } g(x, y) = 2$  everywhere.

### 3. Parametrized curves in the plane

- *Parametrized curve:*  $\mathcal{C} = c(t) = (x(t), y(t))$  for  $a \leq t \leq b$ .  
We can imagine  $c(t)$  as the position at time  $t$  of a particle moving along  $\mathcal{C}$  from the start point  $c(a) = (x(a), y(a))$  to the end point  $c(b) = (x(b), y(b))$ .  $\mathcal{C}$  is a *closed curve* if  $c(a) = c(b)$ .
- *Tangent vector* at point  $c(t)$ :

$$c'(t) = \lim_{\epsilon \rightarrow 0} \frac{c(t + \epsilon) - c(t)}{\epsilon} = (x'(t), y'(t)).$$

Rephrasing: for two points  $c_0 = c(t_0)$  and  $c_1 = c(t_1)$  close together along  $\mathcal{C}$ , the increment vector between them is approximately the velocity vector multiplied by the time increment:

$$c_1 - c_0 \approx c'(t_1) (t_1 - t_0) = c'(t_1) \Delta t_1.$$

- *Example:*  $\mathcal{C} = c(t) = (\cos t, \sin t)$  for  $0 \leq t \leq 2\pi$ , unit circle.  
Tangent vector at  $c(t)$  is:  $c'(t) = (-\sin t, \cos t)$ .  
For  $t = \pi/2$ ,  $c(t) = (0, 1)$ ,  $c'(t) = (-1, 0)$ .

### 4. Circulation around a curve

- We wish to measure the total drag or circulation of  $g(x, y)$  pushing around a closed curve  $\mathcal{C}$ . This is a large-scale version of  $\text{curl } g$ , which measures the rate of circulation of  $g(x, y)$  near a particular point.

- *Drag*: The drag of a constant vector field  $g(x, y) = (c, d)$  along the line segment from  $(0, 0)$  to  $(p, q)$  is the dot-product:

$$(c, d) \cdot (p, q) = cp + dq,$$

the product of vector lengths times cos of the angle between.

- *Circulation line integral of  $g(x, y)$  along  $\mathcal{C}$* . Mark  $N$  points of  $\mathcal{C}$ :

$$c_0, c_1, \dots, c_N = c_0,$$

with  $c_j = c(t_j)$ . We have:

$$c_j - c_{j-1} \approx c'(t_j) (t_j - t_{j-1}) = c'(t_j) \Delta t_j.$$

We can compute the total circulation of  $g(x, y)$  around  $\mathcal{C}$  by adding up the drag along each tiny line segment from  $c_{j-1}$  to  $c_j$ :

$$\begin{aligned} \oint_{\mathcal{C}} g(x, y) \cdot dc &:= \lim_{N \rightarrow \infty} \sum_{j=1}^N g(c_j) \cdot (c_j - c_{j-1}) \\ &:= \lim_{N \rightarrow \infty} \sum_{j=1}^N g(c(t_j)) \cdot c'(t_j) \Delta t_j \\ &= \int_{t=a}^b g(c(t)) \cdot c'(t) dt. \end{aligned}$$

Note that  $g(c(t)) \cdot c'(t)$  is a scalar-valued function of  $t$ , so the last line is an ordinary integral.

- *Example*: Let  $\mathcal{C} = (\cos t, \sin t)$  for  $0 \leq t \leq 2\pi$ , and  $g(x, y) = (1, 0)$  a horizontal constant vector field. Since the drag on top of the curve cancels the opposite drag on the bottom, we expect zero circulation. In fact:

$$\begin{aligned} \oint_{\mathcal{C}} g(c) \cdot dc &= \int_{t=0}^{2\pi} g(\cos t, \sin t) \cdot (\cos' t, \sin' t) dt \\ &= \int_{t=0}^{2\pi} (1, 0) \cdot (-\sin t, \cos t) dt = \int_{t=0}^{2\pi} -\sin t dt = 0. \end{aligned}$$

## 5. Global outflow via line integrals

- We wish to measure the total outflow or flux of  $g(x, y)$  across a closed curve  $\mathcal{C}$ . This is a large-scale version of  $\text{div } g(x, y)$ , which measures the rate of outflow near a particular point.

- *Flux*: The flow of a constant vector field  $g(x, y) = (c, d)$  across a line segment from  $(0, 0)$  to  $(p, q)$  is the cross-product:

$$(c, d) \times (p, q) = cq - dp,$$

the product of vector lengths times sin of the angle between.

- *Flux line integral of  $g(x, y)$  along  $\mathcal{C}$* . As before, we compute the total outflow as:

$$\oint_{\mathcal{C}} g(x, y) \times dc = \lim_{N \rightarrow \infty} \sum_{j=1}^N g(c_j) \times (c_j - c_{j-1}) = \int_{t=a}^b g(c(t)) \times c'(t) dt.$$

- *Example*: Again let  $\mathcal{C} = (\cos t, \sin t)$  and  $g(x, y) = (1, 0)$ . Since inflow on the left should cancel outflow on the right, we expect zero flux. In fact:

$$\oint_{\mathcal{C}} g(c) \times dc = \int_{t=0}^{2\pi} (1, 0) \times (-\sin t, \cos t) dt = \int_{t=0}^{2\pi} \cos t dt = 0.$$

## 6. Green's Theorems: global versus local

- Let  $R$  be a region on the plane whose boundary is a simple closed curve  $\mathcal{C}$  (oriented counter-clockwise). Let  $g(x, y)$  be vector field which is defined and differentiable at every point of  $R$ .
- *Theorem*: The circulation of  $g$  around the boundary curve is equal to the total curl of  $g$  inside the region:

$$\oint_{\mathcal{C}} g(c) \cdot dc = \iint_R \text{curl } g(x, y) dx dy,$$

where the right side is a double integral over the region  $R$ .

- *Theorem*: The flux of  $g$  around the boundary curve is equal to the total divergence of  $g$  inside the region:

$$\oint_{\mathcal{C}} g(c) \times dc = \iint_R \text{div } g(x, y) dx dy.$$

- *Proof*: Divide  $R$  into little regions, and write the total line integral as a sum of line integrals over tiny regions. Inside each tiny region,  $g(x, y)$  can be replaced by its linear approximation, so that we can compute the tiny line integrals to be the area times curl  $g$  or div  $g$ .
- *Corollary*: If  $g(x, y)$  is an electrical force field with curl  $g = \text{div } g = 0$  inside the region  $R$ , then  $g$  has zero circulation and flux over the boundary curve  $\mathcal{C}$ :

$$\oint_{\mathcal{C}} g(c) \cdot dc = \oint_{\mathcal{C}} g(c) \times dc = 0$$