16.7 Surface Integrals

Let f be a function defined on a region of \mathbb{R}^3 that contains the surface S. In this section we will define the surface integral of f over S.

Definition. Suppose that the surface *S* has the vector equation

(1)
$$\mathbf{r}(u,v) = x(u,v)\mathbf{i} + y(u,v)\mathbf{j} + z(u,v)\mathbf{k}, \quad (u,v) \in D$$

Now if the components of \mathbf{r}_u and \mathbf{r}_v are continuous and \mathbf{r}_u and \mathbf{r}_v are nonzero and nonparallel in the interior of D, then we define the **surface integral of** f **over the surface** S by

(2)
$$\iint_{S} f(x, y, z) \, dS = \iint_{D} f\left(\mathbf{r}(u, v)\right) \left|\mathbf{r}_{u} \times \mathbf{r}_{v}\right| \, dA$$

Remark. Compare with the definition of a line integral from section 16.2.

(3)
$$\int_C f(x, y, z) \, ds = \int_a^b f(\mathbf{r}(t)) \left| \mathbf{r}'(t) \right| \, dt$$

Here $\mathbf{r}(t)$ is a smooth parametrization of the space curve *C*.

Example 1. Let b > 0 and let S be the cone with vector equation

$$\mathbf{r}(u,v) = u\cos v \,\mathbf{i} + u\sin v \,\mathbf{j} + u \,\mathbf{k}, \quad 0 \le u \le b, \ 0 \le v \le 2\pi$$

Evaluate the surface integral $\iint_S x^2 z \, dS$.

Now

$$\mathbf{r}_u = \cos v \, \mathbf{i} + \sin v \, \mathbf{j} + \mathbf{k}, \quad \mathbf{r}_v = -u \sin v \, \mathbf{i} + u \cos v \, \mathbf{j}$$

So that

$$\mathbf{r}_u \times \mathbf{r}_v = -u \cos v \, \mathbf{i} + u \sin v \, \mathbf{j} + u \, \mathbf{k}$$

and

$$|\mathbf{r}_u \times \mathbf{r}_v| = \sqrt{u^2 \cos^2 v + u^2 \sin^2 v + u^2}$$
$$= \sqrt{2}u$$

since $u \ge 0$. Thus

(4)
$$\iint_{S} x^{2} z \, dS = \sqrt{2} \iint_{D} \left(u^{2} \cos^{2} v \right) u \cdot u \, dA$$
$$= \sqrt{2} \int_{0}^{b} u^{4} \, du \int_{0}^{2\pi} \cos^{2} v \, dv$$
$$= \frac{\sqrt{2} b^{5}}{5} \int_{0}^{\pi} \frac{1 + \cos 2v}{2} \, dv$$
$$= \frac{b^{5}}{5\sqrt{2}} \left(v + \frac{\sin 2v}{2} \right) \Big|_{0}^{2\pi}$$
$$= \frac{\pi \sqrt{2} b^{5}}{5}$$

Let's rework the previous example with the parametrization (of S) given by the vector equation

$$\mathbf{r}(x,y) = x \,\mathbf{i} + y \,\mathbf{j} + \sqrt{x^2 + y^2} \,\mathbf{k}, \quad x^2 + y^2 \le b^2$$

Then

$$\mathbf{r}_x = \mathbf{i} + \frac{x}{\sqrt{x^2 + y^2}} \mathbf{k}, \quad \mathbf{r}_y = \mathbf{j} + \frac{y}{\sqrt{x^2 + y^2}} \mathbf{k}$$

Thus

$$\mathbf{r}_x \times \mathbf{r}_y = \frac{-x}{\sqrt{x^2 + y^2}} \mathbf{i} + \frac{-y}{\sqrt{x^2 + y^2}} \mathbf{j} + \mathbf{k}$$

and

$$|\mathbf{r}_x \times \mathbf{r}_y| = \sqrt{2}$$

Now

$$\iint_{S} x^2 z \, dS = \sqrt{2} \iint_{D} x^2 \sqrt{x^2 + y^2} \, dA$$

Switching to polar coordinates we obtain

$$=\sqrt{2}\int_{0}^{2\pi}\int_{0}^{b}\left(r^{2}\cos^{2}\theta\right)r\cdot r\,dr\,d\theta$$

which is (4).

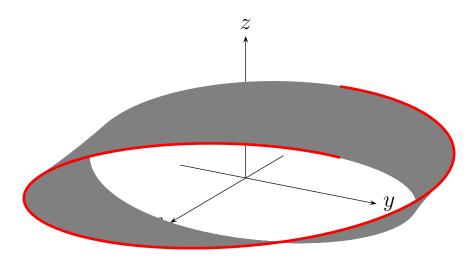
Orientation

We call a smooth surface S orientable or two-sided if it is possible to define a field n of unit normal vectors on S that varies continuously with position.

Smooth surfaces that enclose solids are orientable and by convention, ${\bf n}$ is chosen to point outward. At each point on an orientable surface the vector ${\bf n}$ indicates the positive direction.

Example 2. Nonorientable Surface

The **Mobius Strip** is an example if a nonorientable (or one-sided) surface.



Now let S be a two-sided surface with vector equation

$$\mathbf{r}(u,v) = x(u,v)\,\mathbf{i} + y(u,v)\,\mathbf{j} + z(u,v)\,\mathbf{k}, \quad (u,v) \in D$$

Now suppose that S has a tangent plane at every point (except possibly at a boundary point). Then it is not difficult to show that

$$\mathbf{n}_1 = rac{\mathbf{r}_u imes \mathbf{r}_v}{|\mathbf{r}_u imes \mathbf{r}_v|}$$

and $n_2 = -n_1$ are unit vectors *normal* to the surface *S*.

If S encloses a solid region E, it is conventional that the **positive** orientation is one for which the unit normal vectors point away from E.

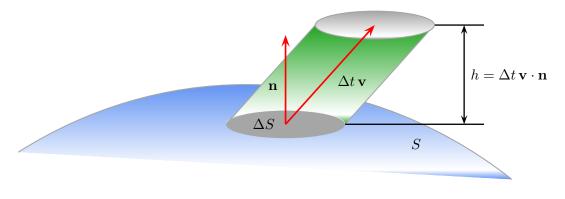


Figure 1: Fluid flow across surface S.

Surface Integrals for Vector Fields

Let *D* be a region in space bounded by a closed surface *S*. Let $\mathbf{v}(x, y, z)$ be the velocity field of a fluid flowing smoothly through *D* and $\delta = \delta(t, x, y, z)$ be the density of the fluid at (x, y, z) at time *t*. Consider the vector field $\mathbf{F} = \delta \mathbf{v}$ and suppose all functions in question have continuous first partial derivatives.

Now consider a small patch ΔS on the surface S (See Figure 1). If Δt is small, then the volume ΔV of fluid that crosses the patch is approximately equal to the volume of a the cylinder with base area ΔS times the height $h = (\Delta t \mathbf{v}) \cdot \mathbf{n}$.

We have

$$\Delta V \approx \mathbf{v} \cdot \mathbf{n} \, \Delta S \, \Delta t$$

So the mass of this volume of fluid is

$$\Delta m \approx \delta \mathbf{v} \cdot \mathbf{n} \, \Delta S \, \Delta t = \mathbf{F} \cdot \mathbf{n} \, \Delta S \, \Delta t$$

It follows that the rate at which mass is leaving the region D across the patch ΔS is roughly

$$\frac{\Delta m}{\Delta t} \approx \mathbf{F} \cdot \mathbf{n} \, \Delta S$$

Summing over S yields

(5)
$$\frac{\sum \Delta m}{\Delta t} \approx \sum \mathbf{F} \cdot \mathbf{n} \Delta S$$

So the right-hand side of this last equation gives an estimate of the average rate at which mass flows across S.

Notice that the right-hand side of (5) is a Riemann sum. So if S and F are nice enough, $\Delta t \rightarrow 0$ and $\Delta S \rightarrow 0$ produces

$$\frac{dm}{dt} = \iint_S \mathbf{F} \cdot \mathbf{n} \, dS$$

This leads to the following definition.

Definition. The Surface Integral of \mathbf{F} over S

If F is a continuous vector filed defined on an oriented surface S with unit normal vector n, then the **surface integral of** F **over** S is

(6)
$$\iint_{S} \mathbf{F} \cdot d\mathbf{S} = \iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS$$

This integral is also called the **flux** of \mathbf{F} across S.

(7)

If S is defined by a vector function $\mathbf{r}(u,v)$ over some domain D , then

$$\mathbf{n} = rac{\mathbf{r}_u imes \mathbf{r}_v}{|\mathbf{r}_u imes \mathbf{r}_v|}$$
 or $\mathbf{n} = -rac{\mathbf{r}_u imes \mathbf{r}_v}{|\mathbf{r}_u imes \mathbf{r}_v|}$

Here we choose the quantity that gives us the preferred direction.

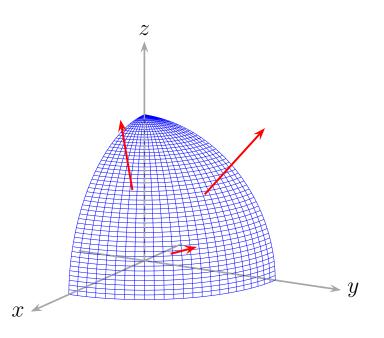
It follows that

$$\iint_{S} \mathbf{F} \cdot d\mathbf{S} = \iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS$$
$$= \iint_{S} \mathbf{F} \cdot \frac{\mathbf{r}_{u} \times \mathbf{r}_{v}}{|\mathbf{r}_{u} \times \mathbf{r}_{v}|} \, dS$$
$$= \iint_{D} \left[\mathbf{F} \left(\mathbf{r}(u, v) \right) \cdot \frac{\mathbf{r}_{u} \times \mathbf{r}_{v}}{|\mathbf{r}_{u} \times \mathbf{r}_{v}|} \right] \, |\mathbf{r}_{u} \times \mathbf{r}_{v}| \, dA$$
$$= \iint_{D} \mathbf{F} \left(\mathbf{r}(u, v) \right) \cdot \left(\mathbf{r}_{u} \times \mathbf{r}_{v} \right) \, dA$$

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Example 3.

Find the flux of the field $\mathbf{F} = y \mathbf{i} + x \mathbf{j}$ across the portion of the sphere $x^2 + y^2 + z^2 = a^2$ in the first octant in the direction away from the origin.



Let $g(x, y, z) = x^2 + y^2 + z^2$. Then the given surface, call it *S*, is just the level surface $g = a^2$. Observe that *S* can defined by the vector equation

$$\mathbf{r}(\phi,\theta) = a\sin\phi\,\cos\theta\,\mathbf{i} + a\sin\phi\,\sin\theta\,\mathbf{j} + a\cos\phi\,\mathbf{k},\ (\phi,\theta) \in D$$

and

$$\mathbf{r}_{\phi} \times \mathbf{r}_{\theta} = a^2 \sin^2 \phi \, \cos \theta \, \mathbf{i} + a^2 \sin^2 \phi \, \sin \theta \, \mathbf{j} + a^2 \sin \phi \, \cos \phi \, \mathbf{k}$$

Here $D = \{(\phi, \theta) : 0 \le \phi \le \pi/2, 0 \le \theta \le \pi/2\}$. (See examples 4 and 10 from section 16.6 in the text.)

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It follows that,

$$\begin{split} \iint_{S} \mathbf{F} \cdot d\mathbf{S} &= \iint_{D} \mathbf{F} \left(\mathbf{r}(u, v) \right) \cdot \left(\mathbf{r}_{u} \times \mathbf{r}_{v} \right) dA \\ &= \iint_{D} \left(a \sin \phi \sin \theta \, \mathbf{i} + a \sin \phi \, \cos \theta \, \mathbf{j} \right) \cdot \\ \left(a^{2} \sin^{2} \phi \, \cos \theta \, \mathbf{i} + a^{2} \sin^{2} \phi \, \sin \theta \, \mathbf{j} + a^{2} \sin \phi \, \cos \phi \, \mathbf{k} \right) \, dA \\ &= a^{3} \int_{0}^{\pi/2} \int_{0}^{\pi/2} \left(\sin^{3} \phi \, \sin \theta \, \cos \theta + \sin^{3} \phi \, \sin \theta \, \cos \theta \right) \, d\phi \, d\theta \\ &= a^{3} \int_{0}^{\pi/2} \sin^{3} \phi \, d\phi \int_{0}^{\pi/2} 2 \sin \theta \, \cos \theta \, d\theta \\ &= \vdots \\ &= \frac{2a^{3}}{3} \end{split}$$

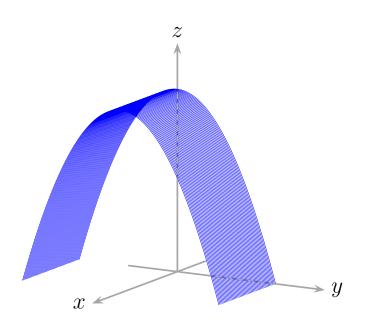
Redo the last example by observing that ${\cal S}$ can also be defined by the vector equation

$$\mathbf{r}(x,y) = x \,\mathbf{i} + y \,\mathbf{j} + \sqrt{a^2 - x^2 - y^2} \,\mathbf{k}, \quad (x,y) \in D,$$

where $D = \{(x, y): x^2 + y^2 \le a^2, x \ge 0, y \ge 0\}.$

Example 4.

Find the flux of the field $\mathbf{F} = z^2 \mathbf{i} + x \mathbf{j} - 3z \mathbf{k}$ outward through the surface cut from the parabolic cylinder $z = 4 - y^2$ by the planes x = 0, x = 1, and z = 0.



Let S be the given parabolic cylinder and $D = \{(x, y) : 0 \le x \le 1, -2 \le y \le 2\}$. Then S can be defined by the vector equation

$$\mathbf{r}(x,y) = x \,\mathbf{i} + y \,\mathbf{j} + (4 - y^2) \,\mathbf{k}, \quad (x,y) \in D$$

Proceeding as usual we have

$$\mathbf{r}_x = \mathbf{i}$$
 and $\mathbf{r}_y = \mathbf{j} - 2y \mathbf{k}$

So that

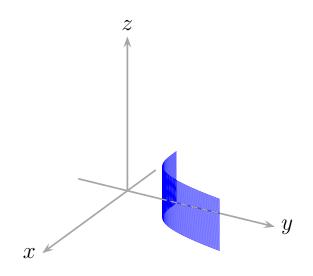
$$\mathbf{r}_x \times \mathbf{r}_y = 2y \, \mathbf{j} + \mathbf{k}$$

Following (7) we obtain

$$\iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS = \iint_{D} \mathbf{F} \left(\mathbf{r}(x, y) \right) \cdot \left(\mathbf{r}_{x} \times \mathbf{r}_{y} \right) \, dA$$
$$= \iint_{D} \left(z^{2} \mathbf{i} + x \mathbf{j} - 3(4 - y^{2}) \mathbf{k} \right) \cdot \left(2y \mathbf{j} + \mathbf{k} \right) \, dA$$
$$= \int_{-2}^{2} \int_{0}^{1} (3y^{2} + 2xy - 12) \, dx \, dy$$
$$= \vdots$$
$$= -32$$

Example 5.

Let *S* be the portion of the cylinder $y = e^x$ in the first octant, with $0 \le x \le 1$ and $0 \le z \le 1$. And let **n** be the unit vector normal to *S* that points away from the *yz*-plane. Find the flux of the field $\mathbf{F} = -2\mathbf{i} + 2y\mathbf{j} + z\mathbf{k}$ across *S* in the direction of **n**.



Let $D = \{(x, z) : 0 \le x \le 1, 0 \le z \le 1\}$. Then *S* can be defined by the vector equation

$$\mathbf{r}(x,z) = x\,\mathbf{i} + e^x\,\mathbf{j} + z\,\mathbf{k}, \quad (x,z) \in D$$

Proceeding as before we have

$$\mathbf{r}_x = \mathbf{i} + e^x \mathbf{j}$$
 and $\mathbf{r}_z = \mathbf{k}$

So that

$$\mathbf{r}_x \times \mathbf{r}_z = e^x \mathbf{i} - \mathbf{j}$$

From (7) we have

$$\iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS = \iint_{D} \mathbf{F} \left(\mathbf{r}(x, z) \right) \cdot \left(\mathbf{r}_{x} \times \mathbf{r}_{z} \right) \, dA$$
$$= \iint_{D} \left(-2 \, \mathbf{i} + 2e^{x} \, \mathbf{j} + z \, \mathbf{k} \right) \cdot \left(e^{x} \, \mathbf{i} - \mathbf{j} \right) \, dA$$
$$= -4 \int_{0}^{1} \int_{0}^{1} e^{x} \, dx \, dz$$
$$= -4 \int_{0}^{1} e^{x} \, dx$$
$$= 4(1 - e)$$

The given surface can also be parameterized by the vector equation

(8)
$$\mathbf{r}_1(y,z) = \ln y \,\mathbf{i} + y \,\mathbf{j} + z \,\mathbf{k}, \quad (y,z) \in D_1$$

Exercise - Set up and evaluate an equivalent integral for Example 5 using the vector equation (8). Of course, you will need to find D_1 .

Example 6. Let b > 0. Find the outward flux of the field

$$\mathbf{F} = \frac{x \,\mathbf{i} + y \,\mathbf{j} + z \,\mathbf{k}}{\rho^3}, \qquad \rho = \sqrt{x^2 + y^2 + z^2}$$

across the surface of the sphere $S: x^2 + y^2 + z^2 = \rho^2 = b^2$.

Notice that the outward normal is

$$\mathbf{n} = \frac{x\,\mathbf{i} + y\,\mathbf{j} + z\,\mathbf{k}}{\sqrt{x^2 + y^2 + z^2}} = \frac{x\,\mathbf{i} + y\,\mathbf{j} + z\,\mathbf{k}}{b}$$

and

$$\mathbf{F} \cdot \mathbf{n} = \frac{x^2 + y^2 + z^2}{b^4} = \frac{1}{b^2}$$

It follows that the flux across the outer surface S is

$$\iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS = \iint_{S} \frac{1}{b^{2}} \, dS = \frac{1}{b^{2}} \iint_{S} dS$$
$$= \frac{1}{b^{2}} \times \text{surface area of } S$$
$$= \frac{1}{b^{2}} 4\pi b^{2} = 4\pi$$

So the outward flux across a sphere of *any* radius for this vector field is 4π . We will have more to say about this example in section 16.9.